STYLUS BASED EVALUATION OF THE SURFACE **ROUGHNESS**

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This paper deals with problems in determining surface roughness values. The process of determining surface roughness values is a relatively difficult task. In this process, it is necessary to set the measurement conditions, which have a huge impact on the measurement uncertainty, and neglecting this process can cause a complete degradation of the measurement and evaluation result. Certain changes in this process are defined by new standards that have been approved to guide this process. The development of the methodology is very necessary in this area in order to obtain reliable data on surface roughness values.

roughness, gauges, uncertainty, calibrator

KEYWORDS

1 INTRODUCTION

This article focuses on the issue of surface roughness assessment. Basically, two large groups of methods are used, i.e., contact methods (also called as stylus-based methods) or non-contact methods for determining surface roughness. Both groups have their advantages and disadvantages. The stylusbased method is a relatively fast contact method that can be implemented using relatively cheaper and more affordable devices and is thus more often used for the process of evaluating surface roughness. However, the non-contact method of determining surface roughness is also more often used in research projects, but it is more expensive in terms of instrumentation and software. In this article, we continue to focus on the stylus-based method (Fig. 1), which is more widespread for ordinary users [EA-4/02 1999, Hogan 2019, Kumar 2019, Suder 2021, Duplak 2023].

Figure 1. Surface roughness tester

In this method (Fig. 2), the touch sensing tip moves along the evaluated surface, and the irregularities that are determined in this way are the basis for processing the values of the individual surface roughness values. Here, however, there is a limitation in that the sensing tip itself has its own dimensions, which affect the process of identifying the unevenness of the surface.

This method therefore has its limitations and cannot capture irregularities smaller than the sensing tip itself. Most surface roughness testers have a stylus tip in the form of a cone with a radius at the end of the tip (Fig. 3).

Figure 3. Stylus tip of surface roughness tester

The terminology and methodology of measurement and evaluation of surface roughness values was established in the standards EN ISO 4287 [ISO 4287: 1997] and EN ISO 5436 [ISO 5436-1: 2000]. In summary, these methods are called Geometrical Product Specifications (GPS). When evaluating the surface roughness, these standards took into account the method of production technology of the evaluated surfaces of the products. When assessing surface roughness values, we therefore distinguished between periodic and non-periodic surface roughness profiles. According to the expected value of arithmetic mean height of roughness (*Ra*) or according to the value of Mean spacing of the profile elements (Rsm) , the

measurement parameters are then determined as a cut-off filter *Lc* or also referred to as (*λc*). This approach has been shown to be discriminatory and in ISO 21920-1, ISO 21920-2, ISO 21920-3 no longer distinguishes between periodic and nonperiodic surface roughness profiles.

In this article, we will further deal with the most frequently evaluated quantity of surface roughness, namely Arithmetical mean height of the roughness (*Ra*).

Surface roughness is a summary characteristic of surface unevenness, which is described by several quantities [ISO 5436- 1: 2000, JCGM 100 2008, JCGM 104 2009, JCGM 200 2012, Whitehouse 2004, Kelemenova 2020, Krenicky 2022]. From the point of view of aesthetics, it affects the overall appearance of the product. In terms of functionality, there are cases when a very small surface roughness is required to reduce friction, for example, or it is necessary to increase the roughness in order to achieve higher braking efficiency. The roughness of the surface is also important as a preparation for surface treatment of products [Straka 2022]. In the field of biomedical engineering of implants, surface roughness is important mainly for better implementation of the implant with living tissues. When it comes to floor coverings, the roughness of the surface is important to prevent people from slipping and falling. The soles of the shoes must also achieve a certain surface roughness. It is equally important to assess the roughness of the surface on road surfaces so that vehicle braking is effective and safe. Surface roughness in mechanical devices such as bearings, pistons in combustion engine cylinders, and the like require as little surface roughness as possible to minimize frictional forces and energy to overcome this friction.

Therefore, the assessment of surface roughness is a key task in many fields and this was the main motivation for creating this work [Koniar 2014, Bozek 2016, Mascenik 2016, Stejskal 2016, Pavlasek 2018, Saga 2019 & 2020, Tlach 2019, Blatnicky 2020, Nikitin 2020, Peterka 2020, Hortobagyi 2021, Kelemen 2021, Kelemenova 2021a,b, Klarak 2021, Kuric 2021, Pivarciova 2021, Lestach 2022, Mikova 2022, Bratan 2023, Fernandez-Lucio 2023, Machac 2023, Romancik 2024, Vagas 2024].

2 SETTING PARAMETERS FOR SENSING SURFACE ROUGHNESS AND EVALUATING SURFACE ROUGHNESS VALUES

The surface profile of the surface roughness is significantly influenced by the production technology used and mostly contains the waviness of the profile, which is the carrier of minor surface irregularities (Fig. 4), which characterize the surface roughness, and which need to be evaluated but without the influence of the waviness of the surface profile. The waviness of the profile is therefore a disturbing influence for the assessment of surface roughness, and it is necessary to remove it from the measured surface profile using a cut-off filter *Lc* and to evaluate this surface profile without this influence of waviness.

Standard surface roughness testers have a cut-off filter setting *Lc* with nominal values of 0.08 mm, 0.25 mm, 0.8 mm, 2.5 mm, 8 mm and 25 mm. The task of the operator is to correctly select the cut-off filter value. Another parameter is the speed of the stylus tip, which can be set to three different values of 0.25 mm/s; 0.5 mm/s; 0.75 mm/s. Furthermore, it is possible to set a specific standard for the evaluation of ISO, DIN, JIS, ANSI, VDA surface roughness values. It is also possible to set other parameters for the data filtering process. All these settings greatly affect the result of the surface roughness evaluation process.

Figure 4. Surface profile with profile waviness and after applying the filter without the effect of surface waviness

Standards ISO 3274 [ISO 3274: 1996], ISO11562 [ISO 11562: 1996] list the recommended values of cut-off filters, stylus tip size and sampling spacing (Tab. 1).

Table 1. Recommended cut-off filter values, stylus tip size and sampling spacing according to ISO 3274, ISO11562 standards

Cut-off λc (mm)	Cut-off λs (μm)	Roughness cut-off wavelength ratio λc / λs	r_{tip} max (μm)	Maximum sampling spacing (μm)	
0.08	2.5	30	2	0.5	
0.25	2.5	100	2	0.5	
0.8	2.5	300	\mathcal{P}	0.5	
2.5	8	300	5	1.5	
8	25	300	10	5	

The EN ISO 4288 standard recommends for non-periodic filter setting profiles and recommends 5 section lsc lengths for the assessment of surface roughness values (Tab. 2). Here the problem arises that in Table 2 there are recommended values for specific values of Ra, which we do not always know, and we want to determine it using the process of measuring the surface profile and evaluating it using a cut-off filter.

Table 2. Recommended filter settings for non-periodic filter profiles for evaluating surface roughness values according to the EN ISO 4288 standard.

Recommendations for setting parameters of the surface roughness tester according to individual standards for nonperiodic profiles are more clearly summarized in graphic form (Fig. 5).

Figure 5. Recommendations for setting parameters of the surface roughness tester according to individual standards for non-periodic profiles

In the case of periodic profiles, the influence of the displacement of the cutting tool during the formation of the surface of the component is more significant, and the influence of waviness is much greater, and therefore, according to the ISO 4288:1996 [ISO 4288: 1996] standard, it is recommended to set the parameters for sensing the surface profile and evaluating the surface roughness values according to the value Mean spacing of the profile elements R sm (Tab. 3).

More clearly, the recommended settings of the surface profile sensing parameters and the evaluation of surface roughness values for periodic surface profiles according to the ISO 4288:1996 standard are summarized in graphic form (Fig. 6).

Table 3. Recommended settings of surface profile sensing parameters and evaluation of surface roughness values for periodic surface profiles according to the ISO 4288:1996 standard

Figure 6. Recommended settings of surface profile sensing parameters and evaluation of surface roughness values for periodic surface profiles according to the ISO 4288:1996 standard.

The ISO 4288:1996 [ISO 4288: 1996] standard was replaced in 2021 by the ISO 21920-3:2021 standard. The whole series of standards ISO 21920-1 [ISO 21920-1: 2021], ISO 21920-2 [ISO 21920-2: 2021], ISO 21920-3 [ISO 21920-3: 2021] introduces no discrimination of periodic and non-periodic profiles of the surface of the evaluated components according to the value of the quantity *Ra* (Tab. 4).

Table 4. Recommended settings of surface profile sensing parameters according to the ISO 21920-3:2021 standard

Setting class Sc	Sc1	Sc2	Sc3	Sc ₄	Sc5
Parameter Ra (µm)	2	Ra≤0.01 0.012 <ra≤0. 0.06<ra≤="" 1.2<ra≤<br="">006</ra≤0.>	1.2	6	Ra > 6
Profile L-filter nesting					
index Nic		0.25	0.8	2.5	8
(cut-off λc (Lc) for R-	0.08				
parameters) (mm)					
Evaluation length Im	0.4			12.5	40
(mm)		1.25	4		
Profile S-filter nesting	0.8		2.5	8	25
index Nis		0.8			
(cut-off λs) (μm)					
Maximum sampling				1.5	5
interval dx (μ m)	0.15	0.15	0.5		
Maximum tip radius r_{tip}		\mathfrak{p}	\mathcal{P}		10
(μm)	2			5	
Section length Isc (mm)	0.08	0.25	0.8	2.5	8
Number of sections nsc	5	5	5	5	5

Recommended settings of surface profile sensing parameters according to the ISO 21920-3:2021 standard is better displayed in graphic form (Fig. 7).

Figure 7. Recommended settings of surface profile sensing parameters according to the ISO 21920-3:2021 standard.

3 EXPERIMENTAL ESTIMATION OF ARITHMETIC MEAN HEIGHT OF ROUGHNESS Ra

According to the standards ISO 21920-1 [ISO 21920-1: 2021], ISO 21920-2 [ISO 21920-2: 2021], ISO 21920-3 [ISO 21920-3: 2021], the methodology for selecting the parameters for measuring the surface profile is uniformly determined for all types of surfaces, but the basic information is the knowledge of the quantity Ra, which we want to determine by this process. One way is to perform measurements at all settings of the surface tester, but this can be extremely laborious and timeconsuming. The second option is to make an initial estimate of the quantity Ra using a non-contact method (Fig. 8) and then choose the correct setting of the measurement and evaluation process accordingly (Fig. 9).

Figure 8. Optical comparison method using a microscope.

In this work, an optical comparison method using a microscope (Fig. 8) was chosen, which enables the simultaneous display of the measured surface and the surface of the surface roughness standard for the relevant type of technology that was used for the product under consideration. The result (Fig. 9) is an approximate value of *Ra*, which is an input parameter in the design of the surface tester setup. This process will significantly

simplify the methodology that is defined in the standards for the geometric specification of products.

Figure 10. Profiles of surface roughness obtained when measuring at the same measurement location under the same conditions but with different cut-off filter settings.

Figure 10 shows a sample of surface roughness for a part made by turning technology. For experimental purposes, the surface profile was measured, and *Ra* was evaluated for all settings of the cut-off filter.

Profiles of surface roughness (Fig. 10) were obtained when measuring at the same measurement location under the same conditions but with different cut-off filter settings (*Lc* = 0.08 mm, 0.25 mm, 0.8 mm and 2.5 mm).

The curves show the influence of waviness on the displayed surface unevenness profile. The most significant effect of the waviness is visible in the last measurement at the largest value of the cut-off filter. Such an analysis is also applicable for determining the appropriate settings of the measurement parameters.

4 CONCLUSIONS

The proposed methodology makes it possible to effectively determine the surface roughness values of the evaluated products. The use of surface roughness estimation is a relatively simple way to solve the problem of determining the parameters for measuring the unevenness profile of the product surface and determining the surface roughness values. An older optical microscope was used, but it is fully functional, so it is a relatively cheap way of solving this process. Sample sheets for various types of technologies were used as standards of surface roughness, which can be quickly confronted with the evaluated surface of the product.

In the future, it will be necessary to verify these samples of surface roughness, and the microscope used will need to be digitized.

In many works, knowing the state of surface roughness is very important because the size of the frictional forces in individual functional surfaces is directly related to it. And so these knowledge will find application in many other works [Vagas 2022, Vagas 2023, Virgala 2022a, Virgala 2022b, Zelnik 2021].

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REFERENCES

- **[Blatnicky 2020]** Blatnicky, M., et al. Design of a Mechanical Part of an Automated Platform for Oblique Manipulation. Applied Sciences, 2020, Vol. 10, No. 23, Art. No. 8467. DOI: 10.3390/app10238467.
- **[Bozek 2016]** Bozek, P., et al. Geometrical Method for Increasing Precision of Machine Building Parts. Procedia Engineering, 2016, Vol. 149, pp. 576-580. https://doi.org/10.1016/j.proeng.2016.06.708.
- **[Bratan 2023]** Bratan, S., Sagova, Z., Saga, M., Yakimovich, B., Kuric, I. New Calculation Methodology of the Operations Number of Cold Rolling Rolls Fine Grinding. Applied Sciences, 2023, Vol. 13, No. 6. eISSN 2076-3417, DOI: 10.3390/app13063484.
- **[Duplak 2023]** Duplak, J., Duplakova, D., Zajac, J. Research on Roughness and Microhardness of C45 Material Using High-Speed Machining. Appl. Sci., 2023, Vol. 13, 7851. https://doi.org/10.3390/app13137851.
- **[EA-4/02 1999]** Expression of the Uncertainty of Measurement in Calibration. European co-operation Accreditation Publication Reference. December 1999.
- **[Fernandez-Lucio 2023]** Fernandez-Lucio, P., Analysis of The Inclination of Slots in Textured Ceramic Tools Through the Study of the Final Roughness and Cutting Forces During Cutting of Cold Work Tool Steel. MM Science Journal, 2023, Vol. November. DOI: 10.17973/MMSJ.2023_11_2023109.
- **[Hogan 2019]** Hogan, R., How to Calculate Linearity Uncertainty. Available online. Cited 2019-06-18. Published 2019-4-8.

https://www.isobudgets.com/how-to-calculatelinearity-uncertainty/.

- **[Hortobagyi 2021]** Hortobagyi, A., et al. Holographic Interferometry for Measuring the Effect of Thermal Modification on Wood Thermal Properties*.* Applied Sciences, 2021, Vol. 11, No. 6. DOI: 10.3390/app11062516.
- **[ISO 4287: 1997]** ISO 4287:1997 Geometrical Product Specifications (GPS)—Surface Texture: Profile Method—Terms, Definitions and Surface Texture Parameters, 1st ed. International Organization for Standardization: Geneve, Switzerland, 1 April 1997.
- **[ISO 4288: 1996]** ISO 4288: 1996 Geometrical Product Specifications (GPS)—Surface Texture: Profile Method—Rules and Procedures for the Assessment of Surface Texture, Edition DIN EN ISO 4288. European Committee for Standardization: Brussels, Belgium, April 1998.
- **[ISO 3274: 1996]** ISO 3274: 1996 Geometrical Product Specifications (GPS)—Surface Texture: Profile Method—Nominal Characteristic of Contact (Stylus) Instruments. European Committee for Standardization: Brussels, Belgium, December 1996.
- **[ISO 5436-1: 2000]** ISO 5436-1:2000 Geometrical Product Specifications (GPS)—Surface Texture: Profile Method, Measurement Standards—Part 1: Material Measures. European Committee for Standardization: Brussels, Belgium, March 2000.
- **[ISO 21920-1: 2021]** ISO 21920-1:2021 Geometrical Product Specifications (GPS)—Surface Texture: Profile—Part 1: Indication of Surface Texture. European Committee for Standardization: Brussels, Belgium, December 2021.
- **[ISO 21920-2: 2021]** ISO 21920-2:2021 Geometrical Product Specifications (GPS)—Surface Texture: Profile—Part 2: Terms, Definitions and Surface Texture Parameters. European Committee for Standardization: Brussels, Belgium, December 2021.
- **[ISO 21920-3: 2021]** ISO 21920-3:2021 Geometrical Product Specifications (GPS)—Surface Texture: Profile—Part 3: Specification Operators. European Committee for Standardization: Brussels, Belgium, December 2021.
- **[ISO 11562: 1996]** ISO 11562:1996 Geometrical Product Specifications (GPS)—Surface Texture: Profile Method—Metrological Characteristics of Phase Correct Filters. European Committee for Standardization: Brussels, Belgium, December 1996.
- **[JCGM 100 2008]** JCGM 100 Evaluation of measurement data – Guide to the expression of uncertainty in measurement (ISO/IEC Guide 98-3). 1st ed., September 2008. Available online: http://www.iso.org/sites/JCGM/GUM-JCGM100.htm
- **[JCGM 104 2009]** *JCGM 104 2009* Evaluation of measurement data – An introduction to the "Guide to the expression of uncertainty in measurement" (ISO/IEC Guide 98-1). 1st ed, July 2009. Available online: http://www.bipm.org/en/publications/guides/gum _print.html.
- **[JCGM 200 2012]** JCGM 200—International Vocabulary of Metrology—Basic and General Concepts and Associated Terms (VIM) 3rd Edition (2008 Version with Minor Corrections). JCGM 2012. Available online: http://www.iso.org/sites/JCGM/VIM-JCGM200.htm.
- **[Kelemen 2021]** Kelemen, M., et al. Head on Hall Effect Sensor Arrangement for Displacement Measurement*.* MM Science Journal, 2021, Vol. October, pp. 4757-4763. DOI: 10.17973/MMSJ.2021_10_2021026.
- **[Kelemenova 2020]** Kelemenova, T., et al. Specific Problems in Measurement of Coefficient of Friction Using Variable Incidence Tribometer. Symmetry, 2020, Vol. 12, 1235. doi.org/10.3390/sym12081235.
- **[Kelemenova 2021a]** Kelemenova, T., et al. Verification of Force Transducer for Direct and Indirect Measurements*.* MM Science Journal, 2021, Vol. October, pp. 4736- 4742. DOI: 10.17973/MMSJ.2021_10_2021021.
- **[Kelemenova 2021b]** Kelemenova, T., et al. Verification of the Torque Gauges*.* MM Science Journal, 2022, Vol. March, pp. 5533-5538. DOI: 10.17973/MMSJ.2022_03_2022014.
- **[Klarak 2021]** Klarak, J., et al. Analysis of Laser Sensors and Camera Vision in the Shoe Position Inspection System. Sensors, 2021, Vol. 21, No. 22, pp. 1-20. DOI: 10.3390/s21227531.
- **[Koniar 2014]** Koniar, D., et al. Virtual Instrumentation for Visual Inspection in Mechatronic Applications. Procedia Engineering, 20114, Vol. 96, pp. 227-234. DOI: 10.1016/j.proeng.2014.12.148.
- **[Krenicky 2022]** Krenicky, T., Olejarova, S., Servatka, M. Assessment of the Influence of Selected Technological Parameters on the Morphology Parameters of the Cutting Surfaces of the Hardox 500 Material Cut by Abrasive Water Jet Technology. Materials, 2022, Vol. 15, 1381.
- **[Kumar 2019]** Kumar, S.P.L. Measurement and uncertainty analysis of surface roughness and material removal rate in micro turning operation and process parameters optimization. Measurement, 2019, Vol. 140. pp. 538-547. doi.org/10.1016/j.measurement.2019.04.029.
- **[Kuric 2021]** Kuric, I., et al. Analysis of Diagnostic Methods and Energy of Production Systems Drives. Processes, 2021, Vol. 9, 843. doi.org/10.3390/pr9050843.
- **[Lestach 2022]** Lestach, L., et al. Two-legged Robot Concepts*.* MM Science Journal, 2022, Vol. October, pp. 5812- 5818. DOI: 10.17973/MMSJ.2022_10_2022091.
- **[Machac 2023]** Machac, T., et al. Aditive Manufacturing of M300 Steel Cutting Tools by Selective Laser Melting. MM Science Journal, 2023, Vol. October, pp. 6735- 6739. DOI: 10.17973/MMSJ.2023_10_2023055.
- **[Mascenik 2016]** Mascenik, J. and Pavlenko, S. Controlled testing of belt transmissions at different loads. MM Science Journal, 2021, Vol. December, pp. 5497- 5501. DOI: 10.17973/MMSJ.2021_12_2021045.
- **[Nikitin 2020]** Nikitin, Y.R., et al. Logical–Linguistic Model of Diagnostics of Electric Drives with Sensors Support. Sensors, 2020, Vol. 20, Iss. 16, pp. 1-19.
- **[Mikova 2022]** Mikova, L., et al. Upgrade of Biaxial Mechatronic Testing Machine for Cruciform Specimens and Verification by FEM Analysis*.* Machines, 2022, Vol. 10, No. 10, 1-29. DOI: https://doi.org/10.3390/machines10100916.
- **[Ostertag 2014]** Ostertag, O., et al. Miniature Mobile Bristled In-Pipe Machine. International J. of Advanced Robotic Systems, 2014, Vol. 11, pp. 1-9. ISSN 1729- 8806. https://doi.org/10.5772/59499.
- **[Pavlasek 2018]** Pavlasek, P., et al. Flexible Education Environment: Learning Style Insights to Increase Engineering Students Key Competences. Edulearn18 Proceedings, 2018.
- **[Peterka 2020]** Peterka, J., et al. Diagnostics of Automated Technological Devices*.* MM Science Journal, Vol. 2020, Vol. October, pp. 4027-4034. DOI: 10.17973/MMSJ.2020_10_2020051.
- **[Pivarciova 2021]** Pivarciova, E., et al. Interferometric Measurement of Heat Transfer above New Generation Foam Concrete*.* Measurement Science Review, 2019, Vol.19, No.4, pp. 153-160. DOI: 10.2478/msr-2019-0021.
- **[Romancik 2024]** Romancik, J., et al. Design, Implementation, And Testing of a 3D printed Gripper Actuated by Nitinol Springs. MM Science J., Vol. June, pp. 7352- 7356. DOI: 10.17973/MMSJ.2024_06_2024009.
- **[Saga 2019]** Saga, M., et al. Contribution to Random Vibration Numerical Simulation and Optimisation of Nonlinear Mechanical Systems. Sci. J. of Silesian Uni. of Technology-Series Transport, 2019, Vol. 103, pp. 143-154. DOI: 10.20858/sjsutst.2019.103.11.
- **[Saga 2020]** Saga, M., et al. Case study: Performance analysis and development of robotized screwing application with integrated vision sensing system for automotive industry. International J. of Advanced Robotic Systems, 2020, Vol. 17, No. 3, pp. 1-23. https://doi.org/10.1177/1729881420923997.
- **[Stejskal 2016]** Stejskal, T., et al. Information Contents of a Signal at Repeated Positioning Measurements of the Coordinate Measuring Machine (CMM) by Laser Interferometer. Measurement Science Review, 2016, Vol. 16, No. 5, pp. 273-279. DOI: https://doi.org/10.1515/msr-2016-0034.
- **[Straka 2022]** Straka, L. and Krenicky, T. Geometric Precision of the Cylinders Surfaces Machined With WEDM Technology. MM Science J., 2022, No. December, pp. 6200-6204. DOI: 10.17973/MMSJ.2022_12_2022146.
- **[Suder 2021]** Suder, J., et al. Experimental Analysis of Temperature Resistance of 3D Printed PLA Components*.* MM Science Journal, 2021, Vol.

March, pp. 4322-4327. DOI: 10.17973/MMSJ.2021_03_2021004.

- **[Tlach 2019]** Tlach, V., et al. Collaborative assembly task realization using selected type of a human-robot interaction. Transportation Research Procedia, 2019, Vol. 40, pp. 541-547. DOI: 10.1016/j.trpro.2019.07.078, 2019.
- **[Vagas 2022]** Vagas, M., et al. Testing of Ethernet-based communication between control PLC and collaborative mechatronic system. In: 20th Int. Conf. on Mechatronics (ME). Pilsen, Czech Republic, 2022. DOI: 10.1109/ME54704.2022.9983428.
- **[Vagas 2023]** Vagas, M., et al. Calibration of an intuitive machine vision system based on an external highperformance image processing unit. In: 24th International Conference on Process Control (PC), Strbske Pleso, Slovakia, 2023, pp. 186-191. DOI: 10.1109/PC58330.2023.10217606.
- **[Vagas 2024]** Vagas, M., et al. Implementation of IO-the Handling and Sorting Sub-Station of the Festo FMS 500 Automated Line. MM Science Journal, 2024, Vol. June, pp. 7348-7351. DOI: 10.17973/MMSJ.2024_06_2024008.
- **[Virgala 2022a]** Virgala, I., et al. Biped Robot with unconventional kinematics*.* MM Science Journal, Vol. 2020, Vol. October, pp. 5819-5824. DOI: 10.17973/MMSJ.2022_10_2022092.
- **[Virgala 2022b]** Virgala, I., et al. A Non-Anthropomorphic Bipedal Walking Robot with a Vertically Stabilized Base. Appl. Sci., 2022, Vol. 12, 4108. https://doi.org/10.3390/app12094108.
- **[Whitehouse 2004]** Whitehouse, D.J. Surfaces and Their Measurement, 1st ed. Butterworth-Heinemann: Oxford, UK, 2004, 432 p. ISBN 9781903996607.
- **[Zelnik 2021]** Zelnik, R., et al. Research and Diagnostics for the Laboratory of Pressure Resistant Sensors*.* MM Science Journal, 2021, Vol. October, pp. 4853-4856. DOI: 10.17973/MMSJ.2021_10_2021041.

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